

Comparative analysis of several sediment transport formulations applied to dam-break flows over erodible beds

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We present a comparative analysis of different sediment transport formulations applied to dam-

Iber is a free shallow water model which solves the 2D depth-averaged shallow water equations break flows over mobile beds. The formulations analyzed include the formulas of Meyer-Peter-

coupled to a turbulence module and a sediment transport module. The model is freely distributed Müller (1948), Wong-Parker (2003), Einstein-Brown (1950), van Rijn (1984), Engelund-Hansen (1967), via www.iberaula.es Yalin (1973) and a general transport formula with ad-hoc coefficients.

Numerical results in two different test cases are presented. The first one consists in an instantaneous dam-break flow over a sand bed, presented in Soares-Frazao et al. (2012). The second one corresponds to the experimental studies performed at the Engineering Faculty of the UNAM **HYDRODYNAMICS HYDRODYNAMICS** (Fuentes-Mariles et al. (2010)) and consists in the erosion of a volcanic sand dike by an overtopping $^{2D \text{ Shallow Water Equations}}$ (1-n) $\frac{\partial Z_b}{\partial q_{\text{sb},x}} + \frac{\partial q_{\text{sb},x}}{\partial q_{\text{sb},x}} + \frac{\partial q_{\text{sb},x}}{\partial q_{\text{sb},x}}$ (Fuentes-Mariles et al. (2010)) and consists in the erosion of a voicanic sand dike by an overtopping (x_x, v_y, h) $(1-p)\frac{\partial D_k}{\partial t} + \frac{\partial D_k}{\partial x} + \frac{\partial D_k}{\partial y}$ $(1-p)\frac{\partial D_k}{\partial t} + \frac{\partial D_k}{\partial x} + \frac{\partial D_k}{\partial y}$

Introduction Model description

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The sediment transport module solves the 2D Exner equation considering both suspended and bed load transport. In the test cases analyzed in this work, only bed load transport was considered

Model performance is analyzed in terms of the bed elevation at the end of the experiment. The best agreement between experimental and numerical data is obtained with Yalin and Meyer-Peter-Muller formulas, both of them give very similar results. The formulas of van Rijn and Wong-Parker underestimate slightly the sediment transport capacity and mobilize less sediment, although the comparison with the experimental results is still good. Einstein-Brown and specially Engelund-Hansen overestimate the sediment transport capacity and give much worse predictions of the bed 3.00 erosion patterns.

All the formulations have been implemented in the numerical model Iber (Bladé et al. (2014)), which solves the depth-averaged shallow water equations coupled to the Exner equation to evaluate the **bed evolution.**

First test case. Dam break over erodible bed (Q_{s,susp}, Q_{s,bed} + Z_{bed}) (visct, k_t, ε) (visct, k_t, ε)

The first one consists in an instantaneous dam-break flow over a sand bed, presented in Soares-Frazao et al. (2012). The bed downstream the dam was made of a well-sorted sand with diameter of 1.61mm, porosity of 0.42 and density of 2.63 kg/m³. The sand layer was completely saturated at the Unam Laboratory experiments on the failure of a small scale sand dyke were conducted at the UNAM beginning of the experiment, and its thickness was 8.55 cm. Upstream water level was 47 cm, while lativitute of Engineering (México). The laboratory model was built in a 5.66 x 0.60 m flume with no

The finite volume mesh is built from 17970 quadrilateral elements of variable size. Average element density of 2.4 kg/m³. size downstream the dam is 33.36 cm², and near the upstream contour 83.55 cm².

Second test case Sand dyke failure by overtopping flow

downstream the water depth was zero.

bed slope. The dam was made of a well-sorted sand with diameter of 0.25mm, porosity of 0.313 and

0.0 **Conclusions** \overline{a} \overline{b} \overline{c} \overline{c}

Experimental data from two different studies of dam break flow over erodible beds has been used to analyze the performance of six commonly used sediment transport formulations. None of these formulations were originally developed for modeling dam break flows, but they are nowadays implemented in many river modeling packages, and used beyond the uniform flow conditions for
(2014). Iber: herramienta de simulación numérica del flujo en ríos. Revista Internacional de Métodos which they were calibrated.

The experimental cases were reproduced with the 2D shallow water model Iber. Despite the The experimental cases were reproduced with the 2D shallow water model Iber. Despite the
Comployity of the bydrodynamic and sodiment transport processes involved in dam broak flows the **Camployity of the hydrodynamic and s** complexity of the hydrodynamic and sediment transport processes involved in dam break flows, the
model gives stable results with all the sediment transport formulations which were tested. Yalin's Caracterización Experiment formula is the only one which gives good numerical predictions in both test cases without any **Soares-Frazão et al.** (2012). Dambreak flows over mobile beds: exp parameter calibration. *Calibration* **Calibration Calibration calibratio**

· Bladé, E., Cea, L., Corestein, G., Escolano, E., Puertas, J., Vázquez-Cendón, M.E., Dolz, J., Coll, A. which they were calibrated. *Numéricos para Cálculo ^y Diseño en Ingeniería*, Vol.30(1), pp.1‐¹⁰

1.5 $\begin{vmatrix} 1 & 0 \\ 0 & 0 \end{vmatrix}$ $\begin{pmatrix} 2 \\ -q_s^* \end{pmatrix} = 5 \cdot (\tau^* - 0.047)^{2,10}$

1.0 $\begin{vmatrix} 1 & 0 \\ 0 & 0 \end{vmatrix}$ $\begin{pmatrix} 4.85 \\ -9.85 \end{pmatrix}$ $\begin{pmatrix} 4.85 \\ -1.0 \end{pmatrix}$

 $\begin{array}{c|c}\n & \text{mean} \\
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\text{mean}\n\end{array}$ a rather precise prediction of the outlet hydrograph, even 2.50 \vert $\qquad \bullet$ UNAM a rather precise prediction of the outlet hydrograph, even $\begin{array}{c|c} \text{1} & \bullet \\ \text{2.00} & \bullet \end{array}$ $\begin{array}{c} \text{1} & \bullet \\ \text{2.00} & \bullet \end{array}$ and $\begin{array}{c} \text{1} & \bullet \\ \text{2.00} & \bullet \end{array}$ and $\begin{array}{c} \text{1} & \bullet \\ \bullet & \bullet \end{array}$ and $\begin{array}{c} \text{1} & \bullet \\ \bullet & \bullet \end{array}$ wong-Parker **net are a multum and all in the raising limb of the hydrograph. All** $\mathbf{E}^{1.50}$ **and** \bullet \bullet Engelund-Hansen the other standard formulas fail to predict the outlet hydrograph. Using the formulations of Meyer‐Peter‐ 0.50 July 2008 Muller, Wong-Parker and Engelund-Hansen, the model under predicts the peak discharge, which means that the $\overline{0.00}$ $\overline{0.00}$ $\overline{0.00}$ $\overline{0.00}$ and $\overline{0.00}$ are $\overline{0.00}$ and $\overline{0.00}$ and $\overline{0.00}$ are $\overline{0.00}$ and $\overline{0.00}$ are $\overline{0.00}$ and $\overline{0.00}$ are $\overline{0.00}$ and $\overline{0.00}$ and $\overline{0.00$ other hand, van Rijn and Einstein-Brown formulas over $\overline{6.00}$ Λ

A generic formula of the type $q_s^* = k \cdot (\tau^* - \tau_c^*)^\alpha$ was calibrated Van Rijn $\begin{vmatrix} A & g$ eneric formula of the type $q_s^* = k \cdot (r^* - r_c^*)^*$ was calibrate by comparing the numerical and experimental and and experimental

E 3.00 $\begin{array}{|c|c|c|c|c|}\n\hline\n\end{array}$ A alin and $\begin{array}{|c|c|c|c|c|}\n\hline\n\end{array}$ by comparing the numerical and experimental
 $\begin{array}{|c|c|c|c|}\n\hline\n\end{array}$ and $\begin{array}{|c|c|c|}\n\hline\n\end{array}$ by comparing the nu α , while keeping the non-dimensional critical shear stress equal to 0.047. Several combinations of parameters *k* and α were found which give a proper prediction of the outlet

s)

Q (l/s

 1.0
 0.5

References

• Soares‐Frazão et al. (2012). Dambreak flows over mobile beds: experiments and benchmark tests for

